

Evaluation of Composite Materials for Heliostat Cost Reduction

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- 1. Motivation
- 2. Reference heliostat model
- 3. Characteristic wind loads
- 4. Selection of pultruded structural composites
- 5. Technoeconomic analysis using equivalent deformation
- 6. Summary and discussion

Motivation

- Composites have become high-volume and mainstream
- DOE cost target: \$50/m²
- Steel is the largest, most volatile material cost in a heliostat
- Challenge: heliostats are a dynamic system with high stiffness requirements

components

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heliostat fiel

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mass production

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integration

Reference heliostat model

- Generic 25m² pedestal-type heliostat
 - Aspect ratio: 1.44
 - Elevation axis height: 2.50m
- Components analyzed:
 - Pylon (blue, 1)
 - Torque tube (green, 2)
 - Facet center support (yellow, 3)
 - Facet end support (blue, 4)
 - Purlin (purple, 5)





Wind loads: base calculation

- Loads per ASTRI Heliostat Design Wind Load Calculator (version v1d; see Emes et al, 2019)
 - Operation: 21 m/s
 - Stow: 45 m/s
 - Turbulence intensity: 26%
 - Chord length: 5m (1:1 aspect ratio)
- Adjustment of wind loads for aspect ratio (AR) using empirical curve fits from Pfahl et al (2011)
 - Operating loads -> evaluate deflection
 - Stow loads -> evaluate factor of safety



Wind load adjustment coefficients from Table 3 of A. Pfahl, M. Buselmeier, and M. Zaschke, "Wind loads on heliostats and photovoltaic trackers of various aspect ratios," Solar Energy, vol. 85, no. 9, pp 2185–2201, Sep. 2011, doi: 10.1016/j.solener.2011.06.006.

Wind load adjustment coefficients for 1.44:1 aspect ratio



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Wind loads: representative distributions

- Source data: University of Adelaide wind tunnel, scale model heliostat, 24 differential pressure taps¹
- Purpose: Quantify transient torques into mirror facet backing structure. Design Wind Load calculator gives summary loads only.

Differential pressure distribution on mirror surface, upright orientation (Pascals)

-49.2	-62.2	-69.8	-79.3	-75.9	-68.5
-56.9	-76.0	-82.9	-91.1	-88.6	-70.2
-51.2	-63.6	-63.6	-73.5	-82.7	-64.3
-45.5	-53.3	-56.6	-54.5	-62.3	-51.0

Differential pressure distribution on mirror surface, stow orientation (Pascals)

-2.1	-5.4	-5.2	-3.5	-4.4	0.1
-3.3	-7.7	-10.3	-16.6	-5.4	-1.6
-4.8	-11.2	-7.0	-4.2	-8.0	-6.5
-40.1	-55.2	-74.8	-53.3	-47.3	-44.1

¹ Wind tunnel data (unpublished) provided by Dr. Matthew Emes, University of Adelaide. "UA heliostat load wind tunnel data NREL"

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Materials and properties

- Baseline: Steel AISI 1020¹
- Composites: Unidirectional fiber pultruded composites (UFPs)
 - Fibers investigated: E-glass², Basalt³, Carbon⁴ •
- UFPs are the lowest-cost, highest-volume, most dimensionally-consistent composites for this application



Comparison of Material Properties, Normalized to Steel (2)



Technoeconomic analysis method

- Worst-case orientation & load
- Re-size each component for pultruded composites
 - Constant shape, total deflection
- Evaluate weight, cost, FOS
- Limits:
 - No change to heliostat design
 - Facets not considered structural
 - First-pass analysis of composites' feasibility; not a comprehensive, dynamic analysis

Sample summary calculation, steel vs glass FRP torque tube

Steel

n	OD (mm)	250.0	513.5
	Wall (mm)	2.7	5.5
	Bending angle (mrad)	1.37	0.25
	Torsion angle (mrad)	0.95	1.65
	Total deflection (mrad)	1.67	1.67
	Cost (\$)	167.33	251.26
al	Weight (kg)	86	92
عدر	FOS	4.3	30.3
е,			

Material



Glass FRP



Results and discussion

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Pylon

- High torsional deflection (twist) at pylon base
- Design for stiffness = overdesign for stress
- Proposed composite material: continuous filament-wound tube



11 10 9 8 7 6 5 4 3 2 1 0 Cost Weight FOS ■ Steel ■ Glass ■ Basalt ■ Carbon

Pylon parameters, 19.06 mrad peak operating deflection

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Torque tube

- High torsional deflection (twist) at elevation drive attachment point
- Continuous filamentwound tube potentially suitable



Torque tube results, 1.67mrad peak operating deflection



compressive (buckling in small flange region) 5.00

 Short length limits deflection

All loads are

Facet center support

• Good fit for pultruded UD composites







Facet end support

- Most deflection is twist at attachment point to purlin
- Result sensitive to mirror stiffness and attachment method to heliostat structure
 - Opportunity to use composite facets



9.00 8.00 7.00 6.00 5.00 4.00 3.00 2.00 1.00 0.00 Cost Weight FOS Steel Glass Basalt Carbon

Facet end support results, 6.63mrad peak local slope deviation

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Purlin

 Most deflection is midspan twist (between attachment to center

& end facet supports)

 Result sensitive to mirror stiffness and attachment method to heliostat structure





Facet backing results, 9.90mrad peak local slope deviation

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Conclusions



- Unidirectional fiber pultrusions (UFPs) lack torsion rigidity for application to pylons, torque tubes for common T-shape designs
- Weaknesses of UFPs indicate the need to study:
 - Structural facets to reduce complexity of supporting assemblies and reduce deflection
 - Advanced pultruded or filament-wound beams for torsional stiffness
 - Lattice and truss structures optimized for low shear modulus of UFP beams





Q&A

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Material property references



1. Steel

- Mechanical properties: "AISI 1020 Steel, cold rolled." https://www.matweb.com/search/datasheet.aspx?matguid=10b74ebc27344380ab16b1b69f1cffbb&ckck=1 (accessed Jul. 06, 2023).
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2. Glass FRP

- Elastic, tensile, and flexural properties: Avient Glasforms 1000 Technical Data Sheet (https://catalog.ides.com/Datasheet.aspx?I=19843&FMT=PDF&E=301883)
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3. Basalt FRP

- Mechanical properties: K. Protchenko, F. Zayoud, M. Urbański, and E. Szmigiera, "Tensile and Shear Testing of Basalt Fiber Reinforced Polymer (BFRP) and Hybrid Basalt/Carbon Fiber Reinforced Polymer (HFRP) Bars," Materials (Basel), vol. 13, no. 24, p. 5839, Dec. 2020, doi: 10.3390/ma13245839.
- Cost estimated equivalent to E-glass FRP based on "Basalt Fiber Properties, Advantages and Disadvantages," Build-on-Prince.com. https://www.princelund.com/basalt-fiber.html (accessed Jul. 01, 2023).

4. Carbon FRP

- Mechanical properties: A. Bussiba, I. Gilad, S. Lugassi, S. David, J. Bortman, and Z. Yosibash, "Mechanical Response and Fracture of Pultruded Carbon Fiber/Epoxy in Various Modes of Loading," Crystals, vol. 12, no. 6, Jun. 2022, Accessed: Jun. 21, 2023. [Online]. Available: https://www.mdpi.com/2073-4352/12/6/850
- Density: Avient Glasforms 2000 Technical Data Sheet (https://catalog.ides.com/Datasheet.aspx?I=19843&FMT=PDF&E=301884)
- Cost: D. Brosius and R. Deo, "Impact of Technology Developments on Cost and Embodied Energy of Advanced Polymer Composite Components," Inst. for Advanced Composites Manufacturing Innovation (IACMI), Knoxville, TN (United States), IACMI/0001-2018/2.5, Jan. 2018. doi: 10.2172/1437162.

Appendix: Composites state of the art

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- Cost of composite materials have generally been too expensive for bulk applications like structural components but cost has reduced significantly
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